

Power Coupler Development for RIA

Spoke Cavity Workshop - Los Alamos National Lab

October 7-8, 2002

Brian Rusnak

Proposed RIA Window/Coupler Design Philosophy



- Mechanical - even a modest coupler needs to be reliable
 - Use common components and geometries to reduce costs
 - Use brazed ceramic windows, Conflats, and VCR fittings over indium wire
 - Design for a warm window to avoid a secondary gas barrier
- RF/Electrical - becomes important if coupler size gets quite small
 - Avoid bellows in RF transmission line to narrow MP resonance bands
 - Design voltage handling of coupler geometry to handle 100% of the full standing wave power levels anticipated for an infinite VSWR condition (4x travelling wave power)
- Thermal - this is a CW coupler
 - Design with a thermal margin of ~200% at nominal operating VSWR
 - Use conductive cooling to thermal intercept circuit where possible to simplify design

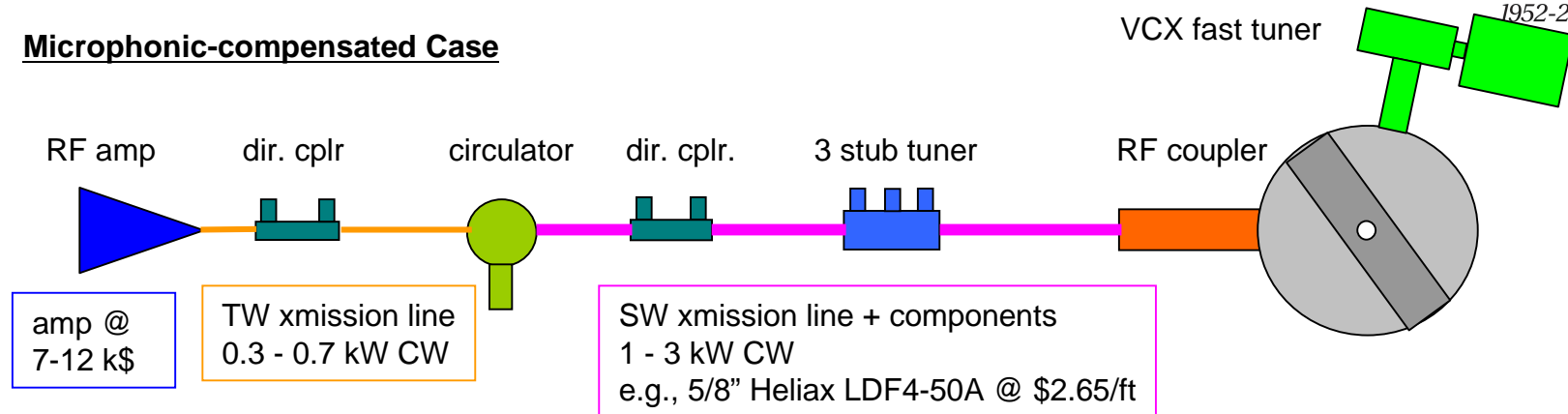
RIA Power Coupler Requirements are Tied to Microphonic and RF Architecture Issues

	numbers needed	frequency range	CW travelling wave (W)	CW standing wave (W)	operating VSWR	coupling approach
compensated micorphonics						
low β driver	276	57.5 - 345 MHz	350 - 700	1,400 - 3,000	1.7	magnetic
high β driver	140	805	2,000 - 6,000	8,000 - 24,000	1.5	electric
overcoupled approach						
low β driver	276	57.5 - 345 MHz	1,000 - 3,000	4,000 - 12,000	5 - 22	magnetic
high β driver	140	805	12,000 - 25,000	48,000 - 100,000	16 - 20	electric

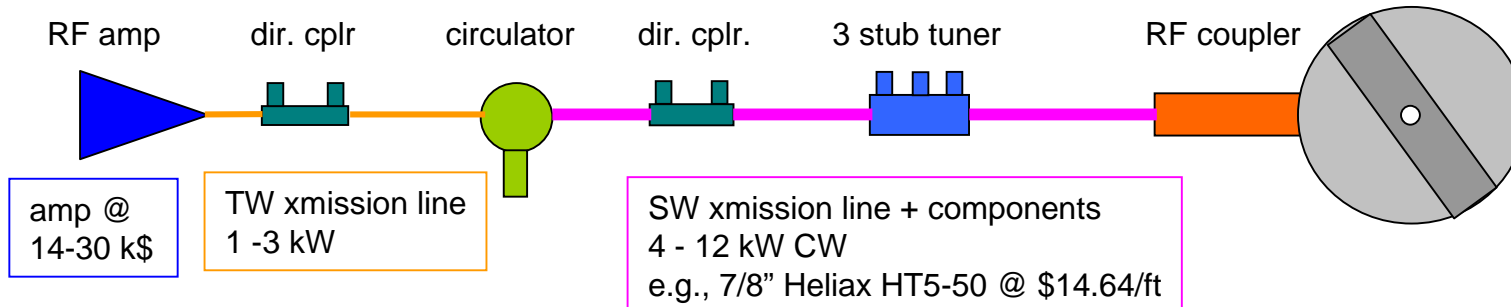
- Reduced (by stiffening) or compensated (by VCX) microphonics allows a smaller RF coupler to be used than the overcoupled case
 - for the low- β driver, the coupler is smaller by a factor of $\sim 3 - 4$
 - for the high- β driver, the factor is $\sim 4 - 6$
- In addition, the larger RF power levels for the overcoupled case impact component cost and size throughout the RF system

Strawman Low- β RF Architecture Designs for RIA

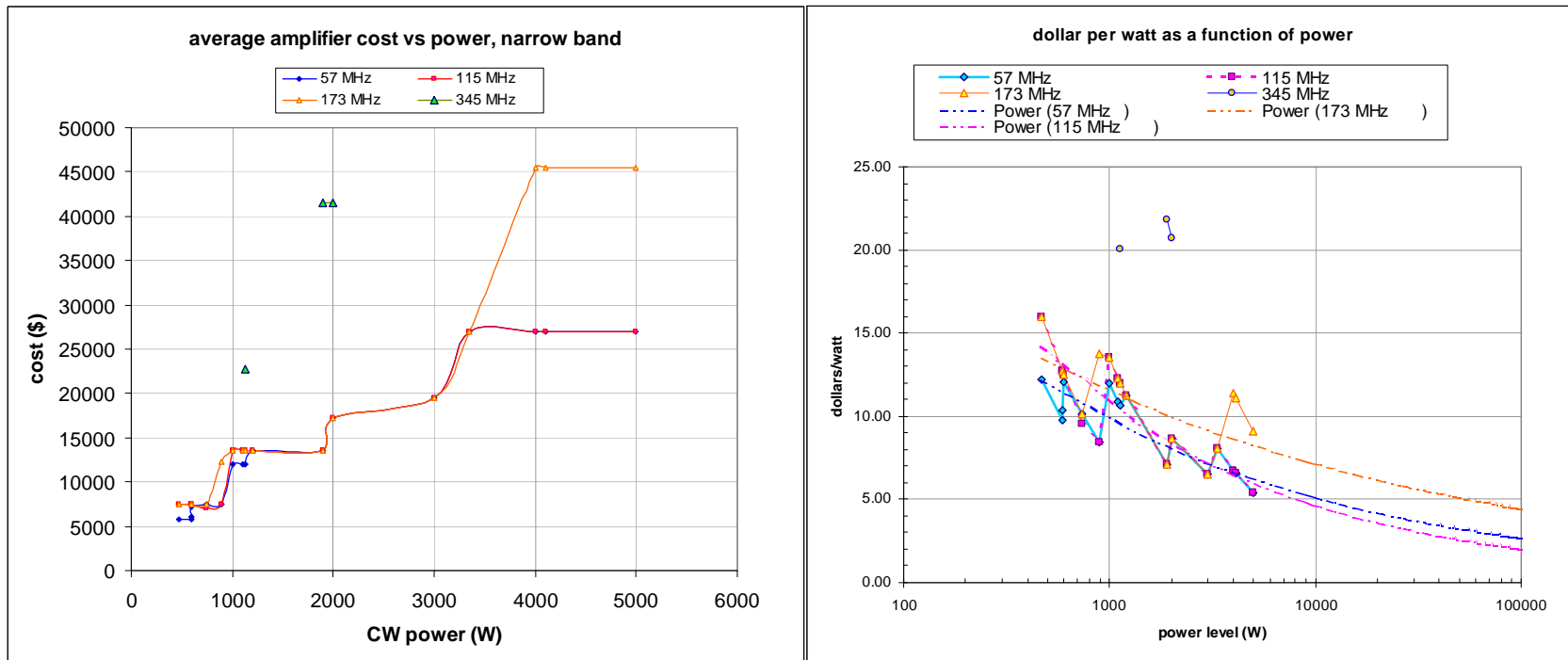
Microphonic-compensated Case



Overcoupled Case



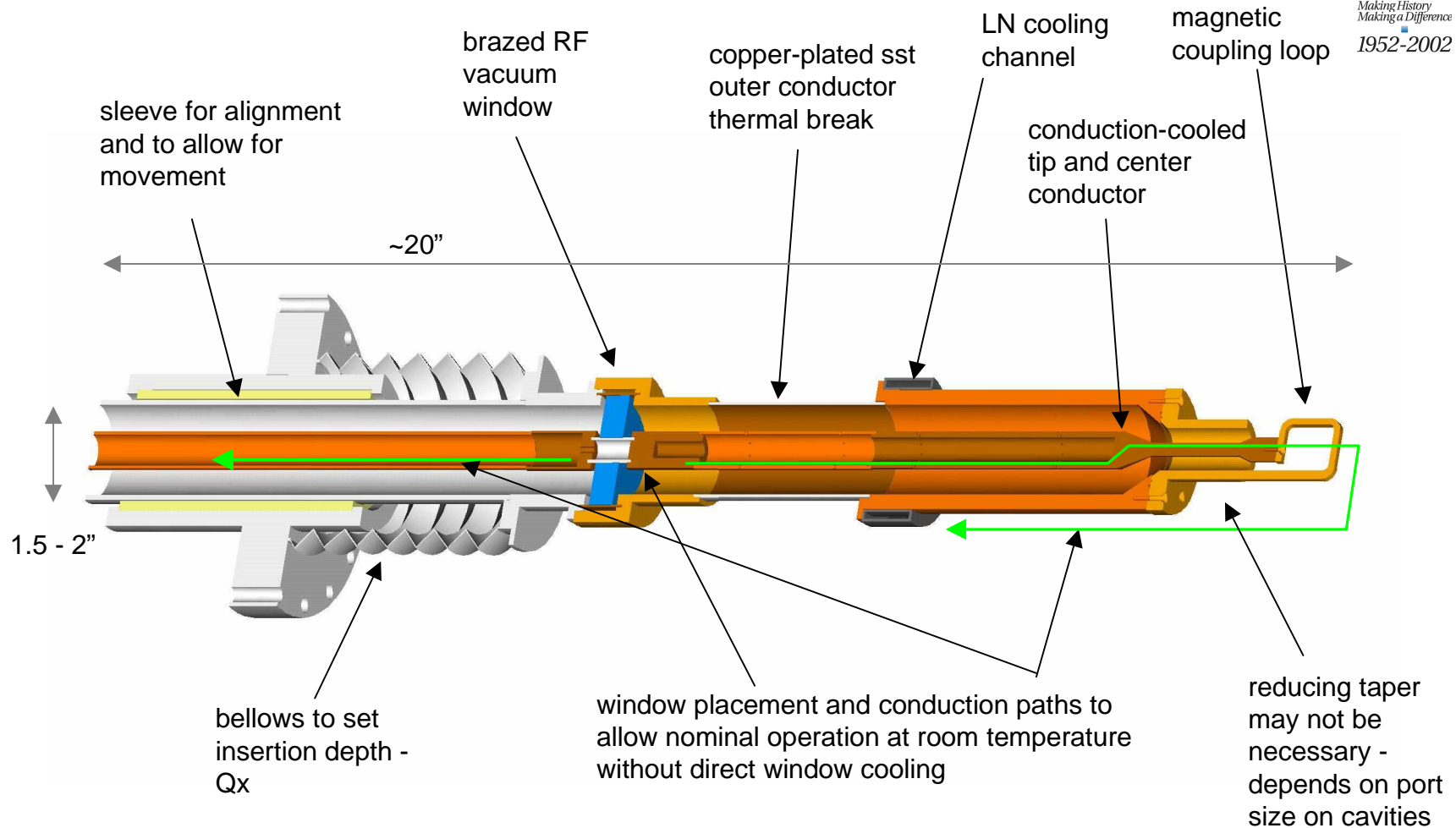
RF Cost Data for Amplifiers, Low and High β Linacs



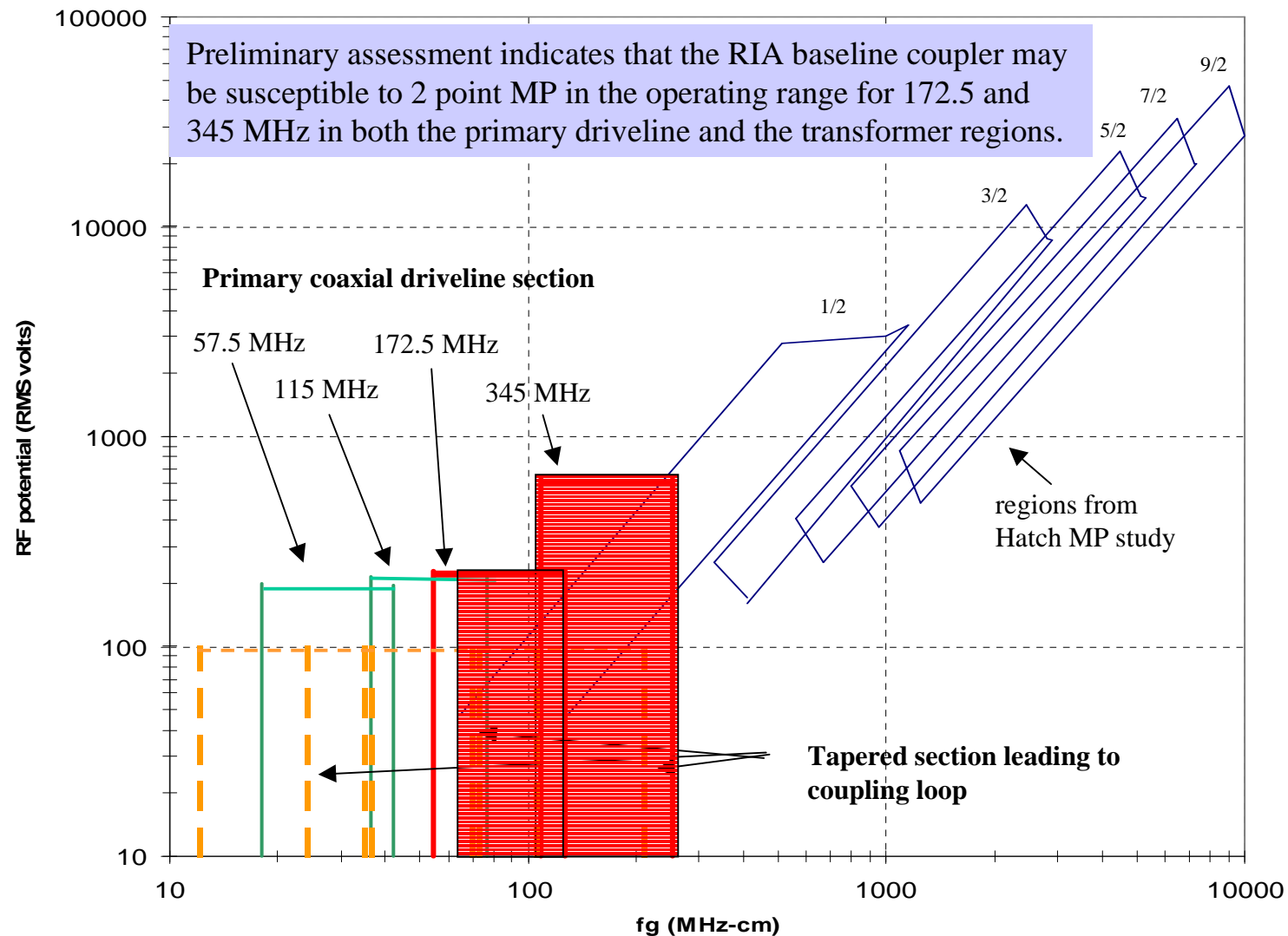
Data used to evaluate RF system costs for the low- β driver linac architectures

Extrapolated \$/Watt numbers used to evaluate RF system costs for the high- β driver linac architectures

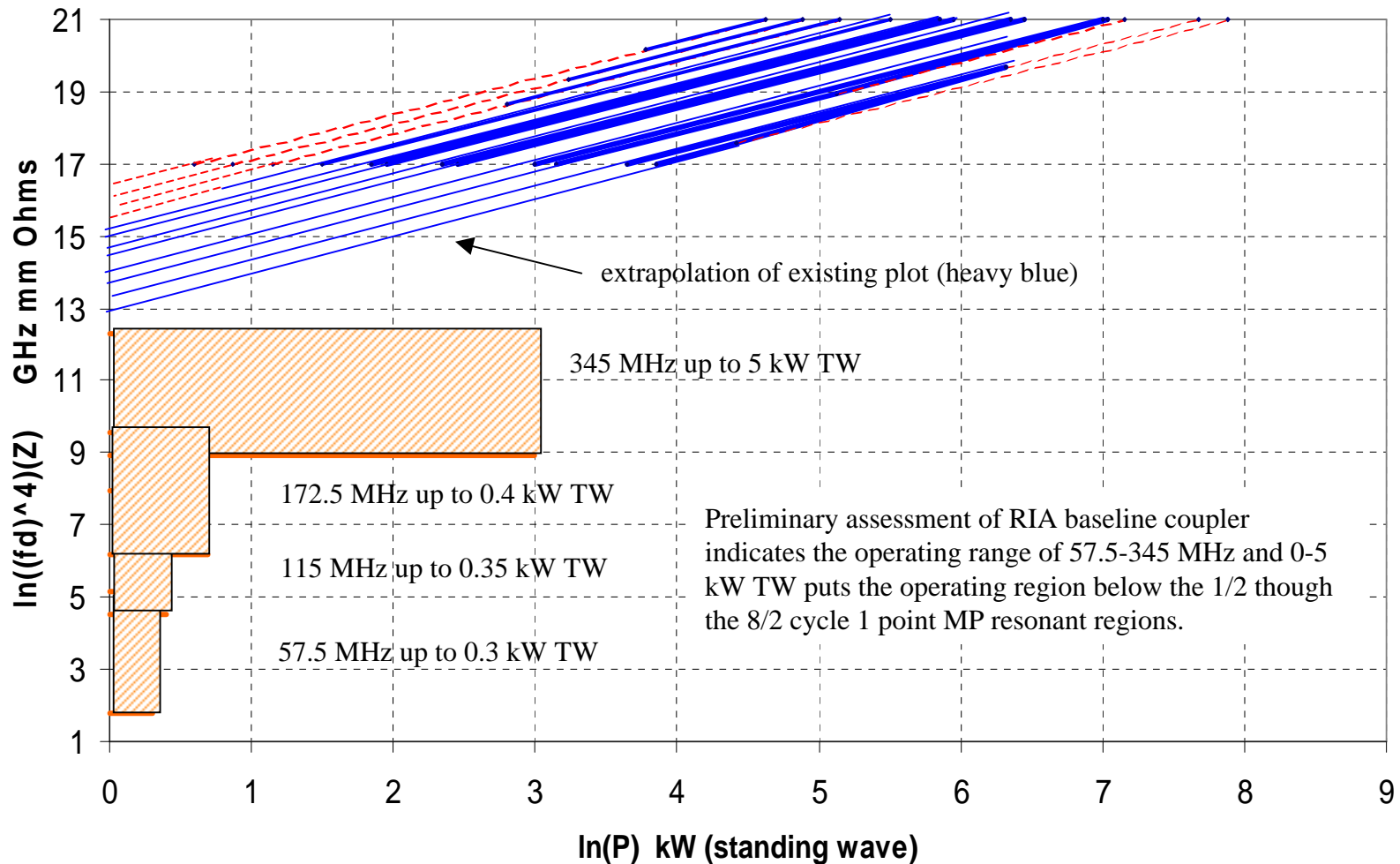
Baseline Design of an RF Coupler for the Low- β Driver Linac



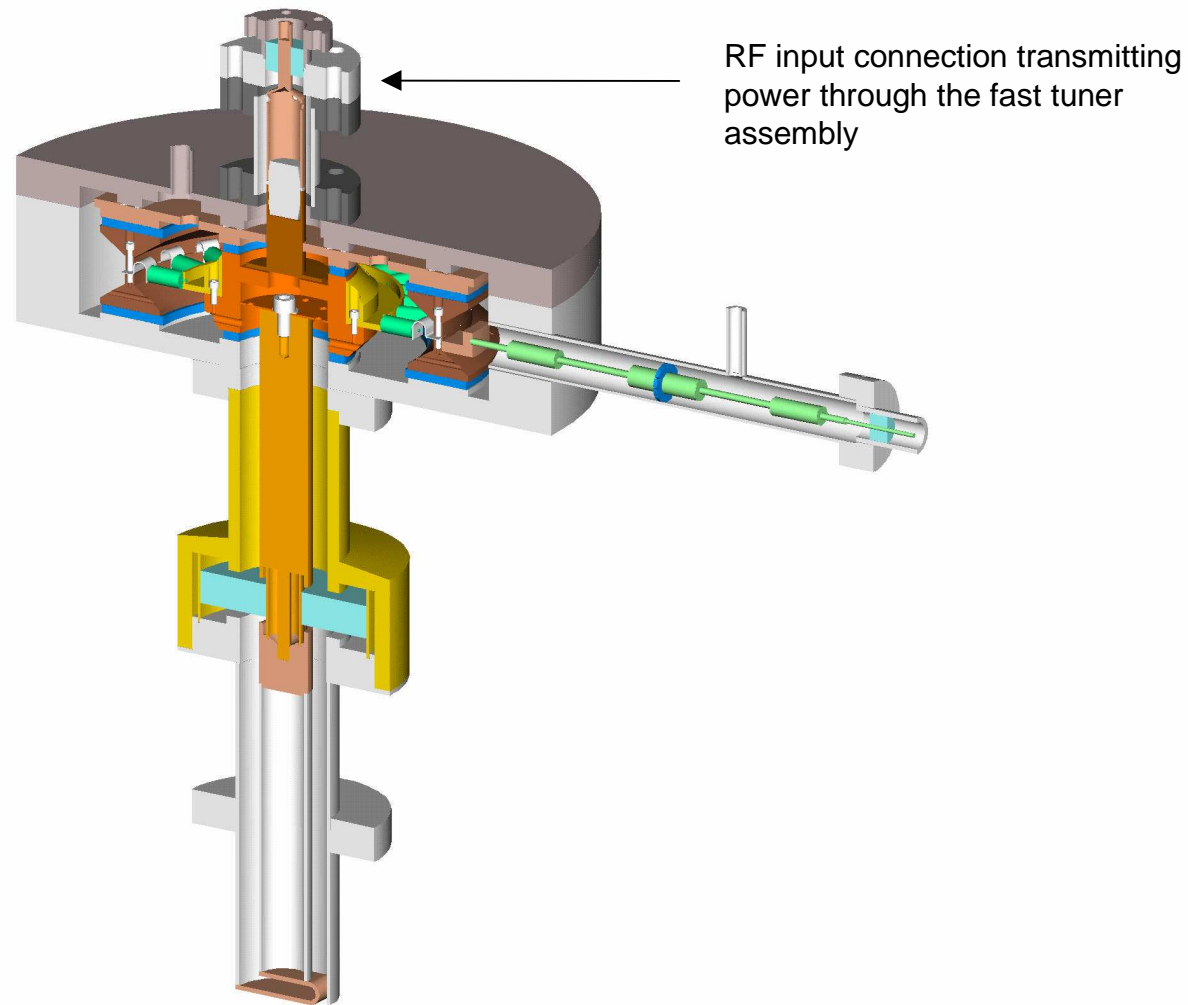
Two Point Multipacting plot from: A.J. Hatch, "Suppression of Multipacting in Particle Accelerators," NIM 41 (1961) pp. 261-277



Reproduction of Somersalo Plot for one point MP in a coax line from: E. Somersalo et al,
 "Analysis of Multipacting in Coaxial Lines," Proceedings of the 1995 PAC, Dallas, TX, May 1-5,
 1995



It May be Possible to Incorporate the RF Drive into the Fast Tuner Assembly



Open Questions (and Discussion Points) on the RIA RF Coupler



- Since the power levels are reasonably low on RIA, is a 3 stub tuner be the best choice to achieve cost effective adjustability?
- Is making “one coupler fits all” the right approach for the low- β driver?
- What is the best common port size for the 4-6 cavities comprising the low- β driver linac? 1.5”, 2”, 2.5”...
- Is the SNS power coupler the best design for the RIA driver elliptical cavities?
 - The average power level is nominally right for TW operation (40 kW), but what about using a stub tuner, or handling mismatches?
 - Lighter beam loading will necessitate modifying the Qx set from SNS
 - How will CW vs. pulsed operation impact thermal intercept temperature choice and refrigerator efficiency?
 - Will saved NRE costs really compensate the technical compromises?